

**Sintering temperature dependency on sodium-ion conductivity for Na<sub>2</sub>Zn<sub>2</sub>TeO<sub>6</sub>  
solid electrolyte**

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**ABSTRACT**

We investigated the sintering temperature dependency on the properties of Na<sub>2</sub>Zn<sub>2</sub>TeO<sub>6</sub> (NZTO) solid electrolyte synthesized via a conventional solid state reaction method. Sintering temperature of calcined NZTO powder, which was obtained by the calcination of precursor at 850 °C, was changed in the range from 650 °C to 850 °C. XRD analysis showed that P2-type layered NZTO phase was formed in all sintered samples without forming any secondary phases. The relative densities of sintered NZTO samples were approximately 83–85 % for the samples sintered at 700 °C or higher. The all sintered samples showed sodium-ion conductivity above 10<sup>-4</sup> S cm<sup>-1</sup> at room temperature and the highest conductivity of 4.0 × 10<sup>-4</sup> S cm<sup>-1</sup> in the sample sintered at 750 °C. The sintering temperature to obtain the highest room temperature conductivity is 100 °C lower than that

used in previous works. Such low sintering temperature compared to other Na-based oxide solid electrolytes could be useful for co-sintering with electrode active materials for fabrication of all-solid-state sodium-ion battery.

**KEYWORDS:** solid electrolyte, layered oxide, sodium-ion conductivity, sintering temperature

## 1. INTRODUCTION

All-solid-state sodium (Na) ion batteries (SiBs) are promising high-safety and low cost alternatives to current lithium (Li) ion batteries (LiBs), particularly suitable for the application to large-scale energy storage systems.<sup>1-5</sup> Development of inorganic solid Na-ion conducting materials used for solid electrolyte is most critical issue to realize all-solid-state SiBs. The solid electrolyte materials should have not only high Na-ion conductivity above  $10^{-3}$  S cm<sup>-1</sup> at room temperature but also chemical and electrochemical stabilities against both positive and negative electrode active materials. Although oxide based solid electrolyte materials have rather lower conductivity and poorer deformability than sulfide based one, they have other advantages such as their chemical stability in air and easiness for handling.<sup>3-5</sup>

Na-ion conducting oxide solid electrolyte Na<sub>2</sub>Zn<sub>2</sub>TeO<sub>6</sub> (NZTO) with a P2-type layered structure is an attractive candidate for the application to all-solid-state SiBs, because of the high ionic conductivity above  $10^{-4}$  S cm<sup>-1</sup> at room temperature range and excellent chemical and electrochemical stability against Na metal.<sup>6-11</sup> NZTO has a honeycomb-structured compound with a space group of *P*6<sub>3</sub>22 and in the layers, every TeO<sub>6</sub> octahedron is surrounded by six ZnO<sub>6</sub> octahedra via edge-sharing. Na ions are

located between the layers at three different sites, all of which are partially occupied and thus Na ions can migrate among them. In addition, the processing temperature of NZTO is much lower than other Na-ion conducting oxides such as Na- $\beta/\beta'$  alumina and NaSICON-type  $\text{Na}_3\text{Zr}_2\text{Si}_2\text{PO}_{12}$ .<sup>12–18</sup>

In the previous works, sintering temperatures of NZTO were commonly set to 850–900 °C.<sup>6–11</sup> However, this sintering temperature may be still high not only for the Na volatilization in the precursor,<sup>10,11</sup> but also for co-sintering with electrode active materials with similar layered structure for fabricating oxide-based solid-state Na batteries.<sup>19–24</sup> In this paper, we investigated the sintering temperature dependency on the properties of NZTO. We controlled the sintering temperatures at 650–850 °C and found that all sintered samples show Na-ion conductivity above  $10^{-4}$  S  $\text{cm}^{-1}$  at room temperature. The maximum room temperature conductivity was achieved when sintering temperature was set to 750 °C.

## 2. EXPERIMENTAL

NZTO was synthesized via a conventional solid state reaction method.  $\text{Na}_2\text{CO}_3$  (Kojundo Chemical Laboratory, 99.5%), ZnO (Kishida Chemical, 99.99%) and  $\text{TeO}_2$  (Kojundo Chemical Laboratory, 99.9%) weighed with the molar ratio of Na : Zn : Te = 2.2 : 2 : 1 (adding 10% excess Na taking into account the volatilization of Na during the processing<sup>10,11</sup>) were mixed and ground with ethanol for 5 hours by planetary ball-milling (Nagao System, Planet M2-3F) with zirconia balls with the diameter of 10 mm in a zirconia pot. The mixture was dried at 80 °C and then calcined at 850 °C for 6 hours in air using a SiC crucible. It is noted that the calcination temperature was set to suppress the formation of O'3-type NZTO phase with much lower Na-ion conductivity than P2-

type one.<sup>10</sup> The calcined NZTO powders were reground and pelletized by cold isostatic pressing at 300 MPa, and then sintered at different temperatures of 650, 700, 750, 800 and 850°C for 12 hours in air using a SiC crucible.

The relative densities of all sintered NZTO were calculated by dividing the mass density by the theoretical one ( $= 4.88 \text{ g cm}^{-3}$ ).<sup>6,7</sup> The crystal phase of each sintered NZTO was evaluated by X-ray diffraction (XRD, RIGAKU Multiflex) using  $\text{CuK}\alpha$  radiation ( $\lambda = 0.15418 \text{ nm}$ ). Microstructure of each sintered NZTO was observed by a scanning electron microscope (SEM, Keyence VE-8800). Ionic conductivity was evaluated at a temperature range from 27 to 127 °C by an AC impedance measurement with a frequency from 4 Hz to 2 MHz and an applied voltage amplitude of 0.1 V, using an impedance meter (HIOKI IM3536). Before the conductivity measurements, both parallel end surfaces of each sintered NZTO pellet were coated with Au films as ion blocking electrodes.

### 3. RESULTS AND DISCUSSION

XRD patterns for calcined NZTO powder (before sintering) and all NZTO samples with different sintering temperatures are shown in Figure. 1. The calculated patterns for P2-type and O'3-type NZTO phases based on their structure data are also plotted as the references.<sup>6,10</sup> Although the diffraction peaks of the crystal plane with a *c*-axis orientation are emphasized slightly, the peak position from main phase for all sintered samples agrees well with the calculated pattern for P2-type NZTO phase. It is confirmed that the contamination of O'3 phase was negligible, because only the sintering temperatures were changed in the range from 650 to 850 °C but the calcination temperature of the mixture of starting materials was fixed to 850 °C.<sup>10</sup>

Figure 2 shows the relative density of NZTO samples plotted against the sintering

temperatures. The relative densities of NZTO samples sintered at 700 °C or higher were ranged in 83–85 % but the density of the sample sintered at 650 °C is much lower than others, indicating that the densification of NZTO promotes at temperature above 700 °C in a conventional solid-state reaction process. SEM images of fractured cross sectional surfaces for all NZTO samples are summarized in Figure 3. NZTO sample sintered at the lowest temperature of 650 °C are mainly composed of small grains with the size of 1–5  $\mu\text{m}$  (Figure 3(a)). Although the relative densities for the samples sintered at 700 °C or higher were nearly the same level, several large grains with the size of 10  $\mu\text{m}$  are confirmed in the sample sintered at 850 °C (Figure 3(e)).

Figure 4(a)–(e) shows the Nyquist plots for electrochemical impedance for all sintered NZTO samples at room temperature (27°C). Here,  $Z'$  in a horizontal axis and  $Z''$  in a vertical axis are the real and imaginary parts of impedance, and the units for both components are  $\Omega\text{ cm}$  for direct comparison among the samples with different geometrical parameters. It is evident that the plots for all samples are composed of the part of a distorted semicircle at frequency range above several 10 kHz and a linear tail at low frequency range. These data belong to the ionic conduction at NZTO grain boundaries and the response by ionic blocking electrodes, respectively.<sup>11</sup> The characteristic frequencies at which the  $Z''$  value shows the maximum in a distorted semicircle part are confirmed to be in the range from 0.5 to 0.9 MHz. Since the upper limit of measurement frequency in this work was limited to 2 MHz, the data reflecting the ionic conduction in NZTO grain is not observed clearly. The dashed lines in the graphs (a)–(e) represent the fitting curves for the complex impedance data for the ionic conduction at grain-boundary and the diameter of the fitting line corresponds to the grain-boundary resistivity  $R_{\text{gb}}$  in each sample.  $R_{\text{gb}}$  for the sample sintered at 650 °C is estimated

to be 3600  $\Omega$  cm and much larger than other samples, due to the lowest relative density and poor connectivity among the grains. As the sintering temperature increases to 750 or 800  $^{\circ}\text{C}$ ,  $R_{\text{gb}}$  decreases to 1100–1200  $\Omega$  cm. The reduction of  $R_{\text{gb}}$  with increasing the sintering temperature below 800  $^{\circ}\text{C}$  is caused by the densification and improvements in intergranular connectivity. At the sintering temperature of 850  $^{\circ}\text{C}$ , however,  $R_{\text{gb}}$  is estimated to be approximately 2000  $\Omega$  cm and becomes larger than the samples sintered at 750 or 800  $^{\circ}\text{C}$ . Increase in  $R_{\text{gb}}$  observed in the sample sintered at 850  $^{\circ}\text{C}$  may be caused by the formation of very small amounts of secondary phases formed on the NZTO grain surface due to excess Na volatilization from grains reported in our previous work.<sup>11</sup> The capacitance  $C_{\text{gb}}$  at grain boundary for each sintered NZTO sample is calculated using the relation  $C_{\text{gb}} = (2\pi f_{\text{max}} R_{\text{gb}})^{-1}$  (unit of  $R_{\text{gb}}$  is  $\Omega$  and  $f_{\text{max}}$  is characteristic frequency) and estimated to be  $10^{-10}$ – $10^{-9}$  F, which is typical capacitance value for grain-boundary in polycrystalline ceramic materials.

The intercept point of an extrapolation line of the linear tail in low frequency range and horizontal  $Z'$  axis corresponds to the total (grain + grain boundary) resistivity  $R_{\text{total}}$  of each sample. The effect of sintering temperature on the  $R_{\text{gb}}$  contribution in  $R_{\text{total}}$  are shown in Figure. 4(f). The  $R_{\text{gb}} / R_{\text{total}}$  value in sintered NZTO shows the maximum (= 0.74) at sintering temperature of 650  $^{\circ}\text{C}$  and minimum (= 0.54) at sintering temperature of 750 or 800 $^{\circ}\text{C}$ . Since the contribution of  $R_{\text{gb}}$  in  $R_{\text{total}}$  for sintered NZTO is large, the magnitude relationship of  $R_{\text{total}}$  among the samples are determined by the difference in  $R_{\text{gb}}$ . As results,  $R_{\text{total}}$  shows the maximum (= 4900  $\Omega$  cm) in the sample sintered at 650  $^{\circ}\text{C}$  and the minimum (= 2500  $\Omega$  cm) in the sample sintered at 750  $^{\circ}\text{C}$ . The grain resistivity  $R_{\text{b}}$  in each sample is roughly estimated to 1100–1300  $\Omega$  cm from by subtracting  $R_{\text{gb}}$  from  $R_{\text{total}}$ . The difference in  $R_{\text{b}}$  among the samples is not so large compared to  $R_{\text{gb}}$ , suggesting that the

ionic conductivity of NZTO grain is not influenced so much by the sintering temperature.

Total (grain + grain boundary) ionic conductivity  $\sigma_{\text{total}}$  of each NZTO sample is calculated by the  $R_{\text{total}}$  value estimated in Figure. 4. Figure. 5(a) shows variation of the product of  $\sigma_{\text{total}}$  and measurement temperature  $T$  for all sintered NZTO as a function of inverse of temperature  $T$ . It is confirmed that the temperature dependence of  $\sigma_{\text{total}}$  in each sample is well expressed by the Arrhenius equation  $\sigma_{\text{total}}T = \sigma_0 \exp(-E_a / k_B T)$ . Here,  $\sigma_0$  is constant,  $E_a$  is activation energy of conductivity and  $k_B$  is Boltzmann constant ( $= 1.381 \times 10^{-23} \text{ J K}^{-1}$ ), respectively.  $E_a$  of each sample can be estimated from the slope of  $\sigma_{\text{total}}T$  in Figure. 5(a).  $E_a$  tends to decrease with increasing the sintering temperature and shows the minimum ( $= 0.25 \text{ eV}$ ) in the sample sintered at  $850 \text{ }^\circ\text{C}$ , but the difference among the samples are not so large.  $\sigma_{\text{total}}$  at  $27 \text{ }^\circ\text{C}$  and  $E_a$  for sintered NZTO are also shown in Figure. 5(b), plotted against the sintering temperatures. As shown in Figure. 4, the difference in  $\sigma_{\text{total}}$  of sintered NZTO samples are mainly caused by the difference in ionic conduction at the grain boundary depending on the sintering temperature.  $\sigma_{\text{total}}$  shows the maximum ( $= 4 \times 10^{-4} \text{ S cm}^{-1}$ ) in the samples sintered at  $750 \text{ }^\circ\text{C}$ , which is  $100 \text{ }^\circ\text{C}$  lower than the condition in previous works.<sup>6-11</sup> Such low sintering temperature compared to other Na-based oxide solid electrolytes could be useful for co-sintering with electrode active materials with similar layered structure for fabricating oxide-based all-solid-state SiBs.<sup>19-24</sup> Even for the sample sintered at the lowest temperature of  $650 \text{ }^\circ\text{C}$ ,  $\sigma_{\text{total}} = 2 \times 10^{-4} \text{ S cm}^{-1}$  was obtained. The lowest  $\sigma_{\text{total}}$  of this sample is attributed to the largest grain boundary resistance (Figure. 4(a)), due to the lowest density and poor connectivity among the grains.  $\sigma_{\text{total}}$  for the sample sintered at  $850 \text{ }^\circ\text{C}$  was  $3.2 \times 10^{-4} \text{ S cm}^{-1}$  and slightly lower than the maximum value because of the increase in grain boundary resistance (Figure.

4(e)).

#### **4. CONCLUSION**

In conclusion, the sintering temperature dependency on the property for NZTO solid electrolyte was investigated. Sintering temperature of NZTO powder was changed in the range between 650 °C and 850 °C. XRD analysis showed that P2-type layered NZTO phase were formed for all sintered samples. When the sintering temperatures is above 700 °C, the relative densities of NZTO samples attained to 83–85 %. The all sintered samples showed Na-ion conductivity well above  $10^{-4}$  S cm<sup>-1</sup> at room temperature and the highest conductivity of  $4.0 \times 10^{-4}$  S cm<sup>-1</sup> was obtained in the samples sintered at 750 °C. The sintering temperature to obtain the highest room temperature conductivity is 100 °C lower than that used in previous works for NZTO, and such low sintering temperature could be useful for co-sintering with electrode active materials in oxide-based all-solid-state SiBs.

#### **ACKNOWLEDGEMENTS**

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## FIGURE CAPTIONS

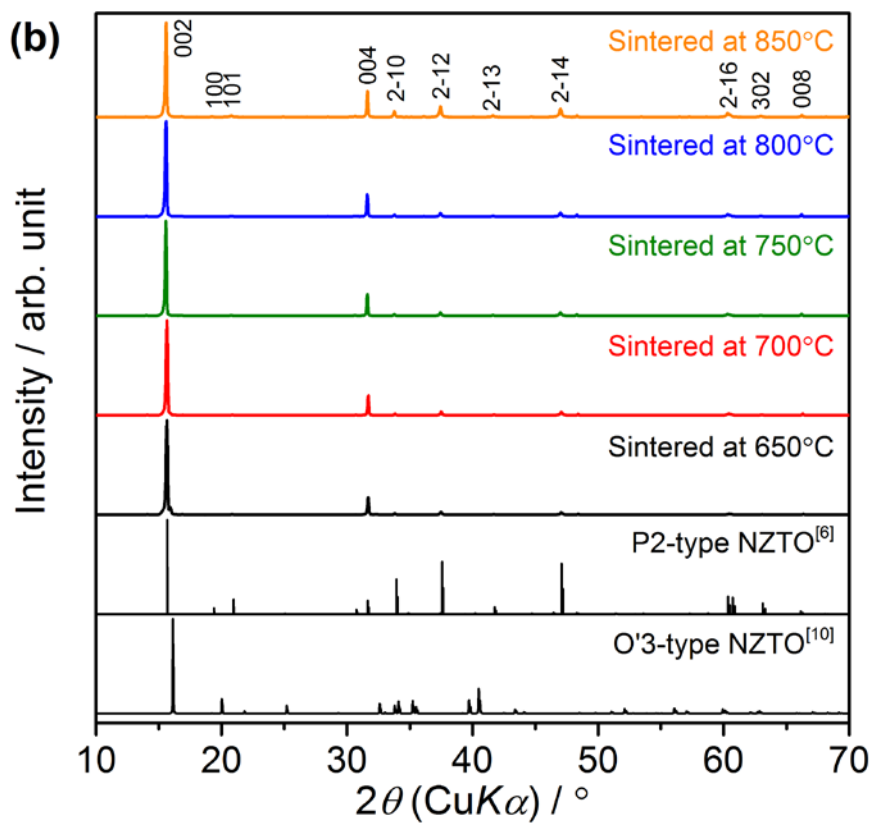
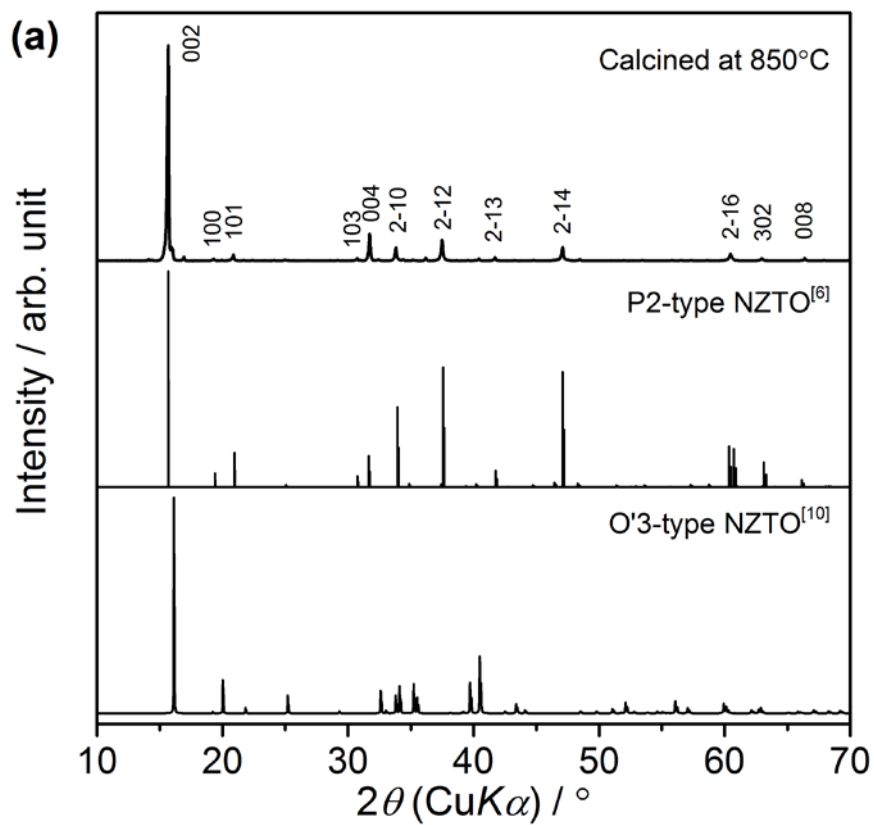
**FIGURE 1.** XRD patterns of (a) calcined NZTO powder (before sintering) and (b) NZTO sintered at different temperatures. Calculated patterns for P2-type and O'3-type NZTO phases are also plotted in each graph.<sup>6,10</sup>

**FIGURE 2.** Relative densities of NZTO plotted against the sintering temperatures. Theoretical density of  $4.88 \text{ g cm}^{-3}$  are used for the calculation.<sup>6,7</sup>

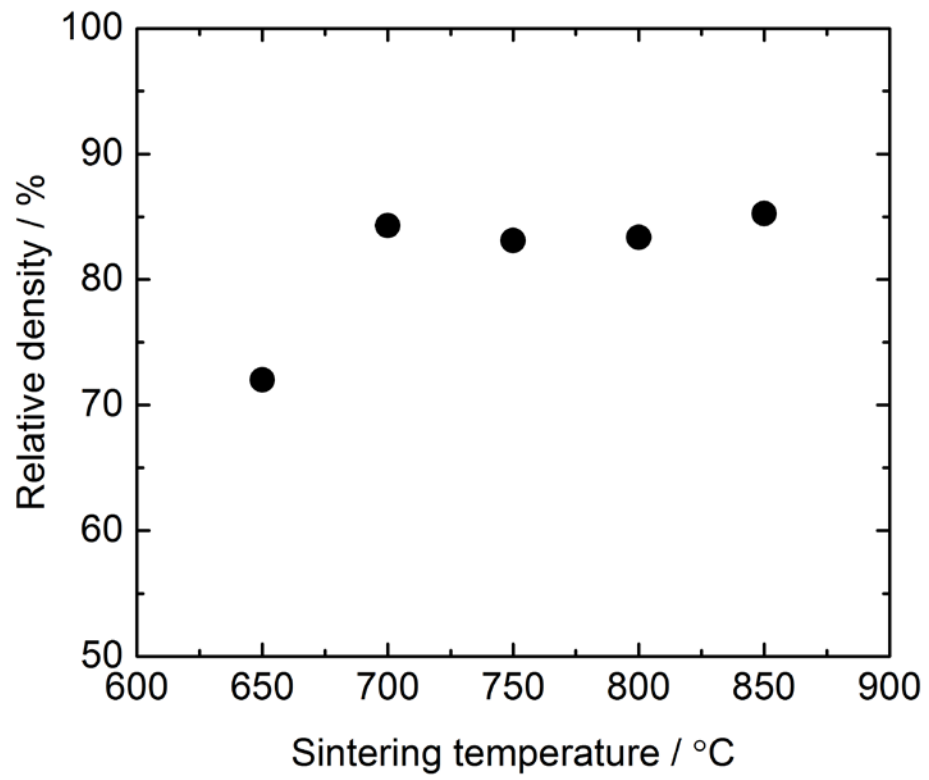
**FIGURE 3.** SEM images for fractured surface microstructures of NZTO sintered at different temperatures: (a) 650 °C, (b) 700 °C, (c) 750 °C, (d) 800 °C and (e) 850°C.

**FIGURE 4.** Nyquist plots of AC impedance at 27°C for NZTO sintered at different temperatures: (a) 650 °C, (b) 700 °C, (c) 750 °C, (d) 800 °C and (e) 850 °C. The dashed lines in the graphs (a)–(e) are the fitting curves for the complex impedance data at grain-boundary ionic conduction. The contribution of  $R_{gb}$  in  $R_{total}$  is also plotted against the sintering temperature in (f).

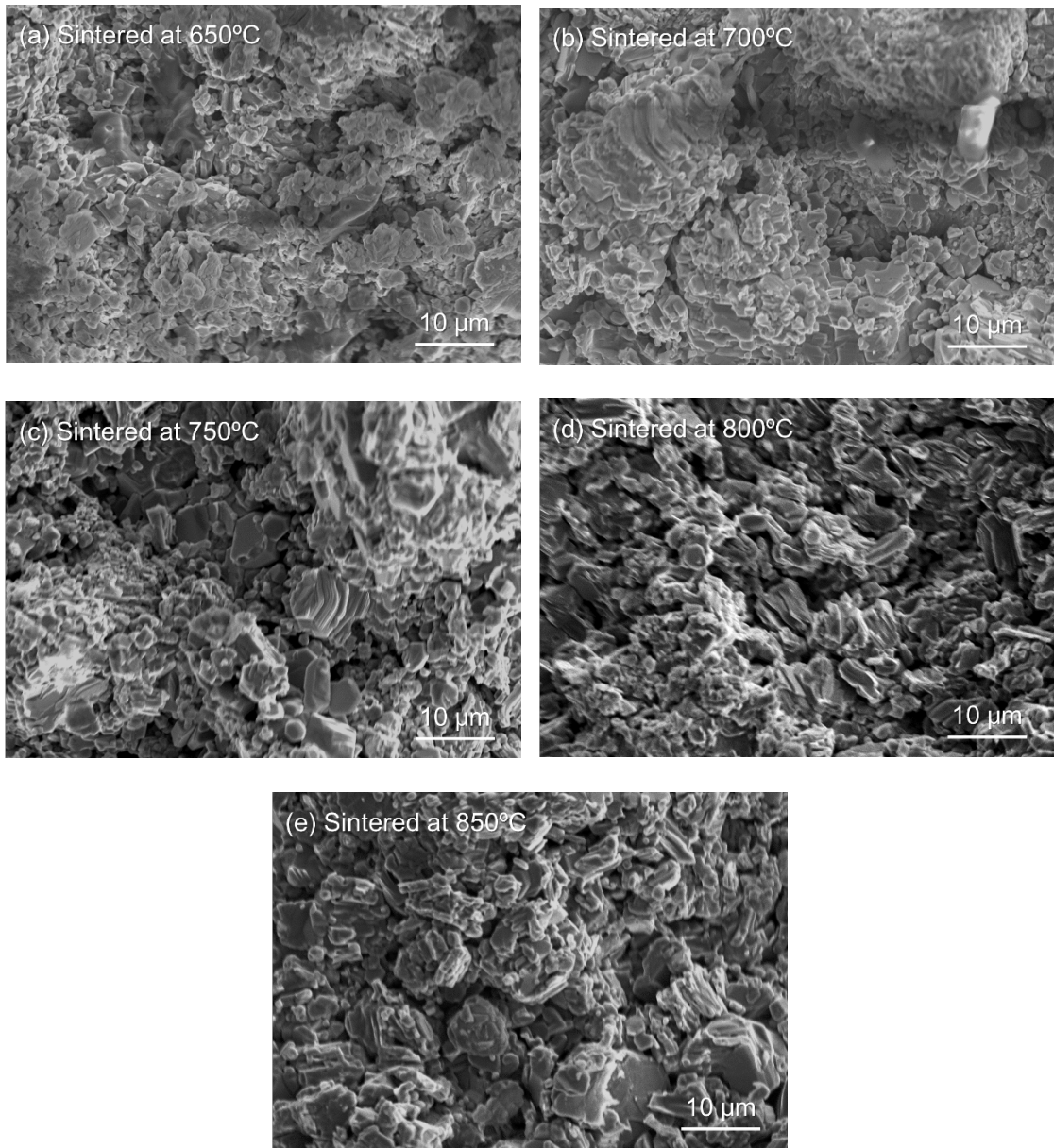
**FIGURE 5.** (a) Arrhenius plots for all sintered NZTO with different sintering temperatures. The conductivity at 27°C and activation energy for NZTO are also shown in (b), plotted against the sintering temperatures.



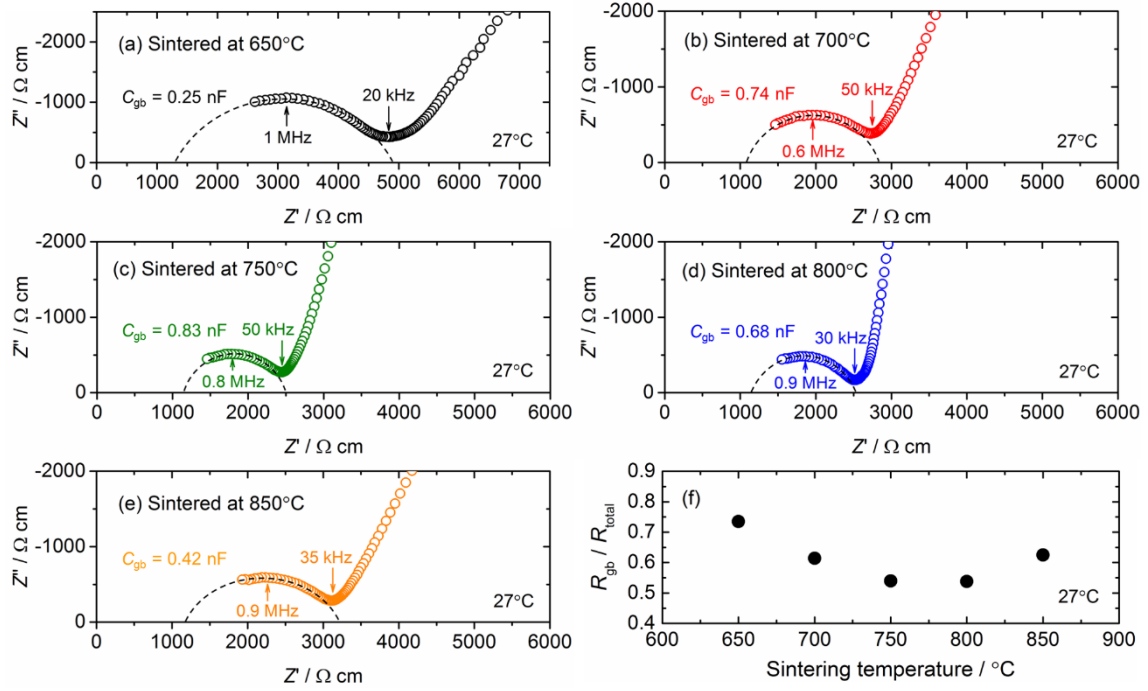
**FIGURE 1**



**FIGURE 2**

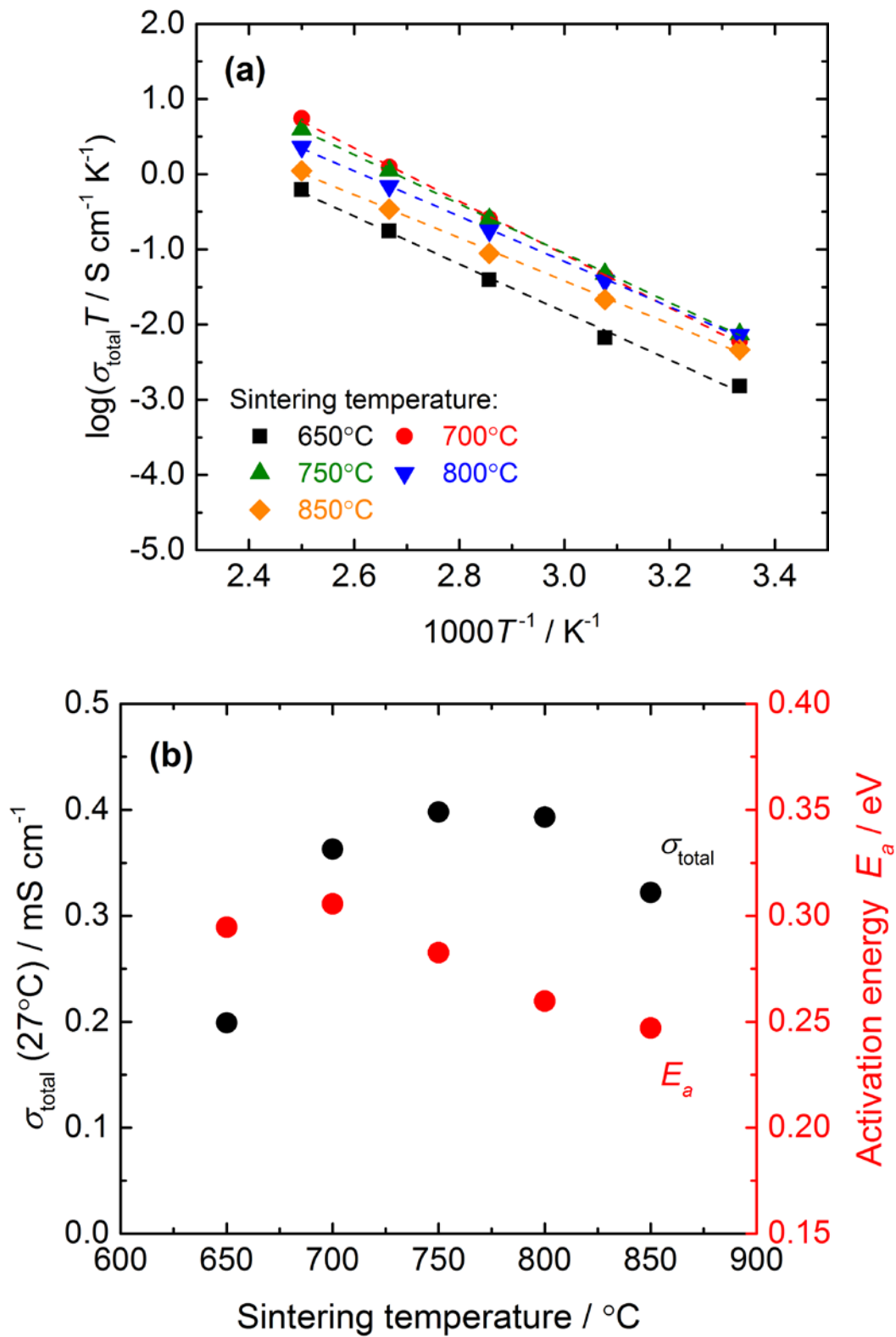


**FIGURE 3**



**FIGURE 4**





**FIGURE 5**